



Modelling of concrete/clay interaction :

taking into account complex mineralogy
influence of non-saturated conditions
and temperature effects

F. Claret, A. Burnol, S. Gaboreau, N. Marty,
C. Tournassat, P. Blanc, EC. Gaucher

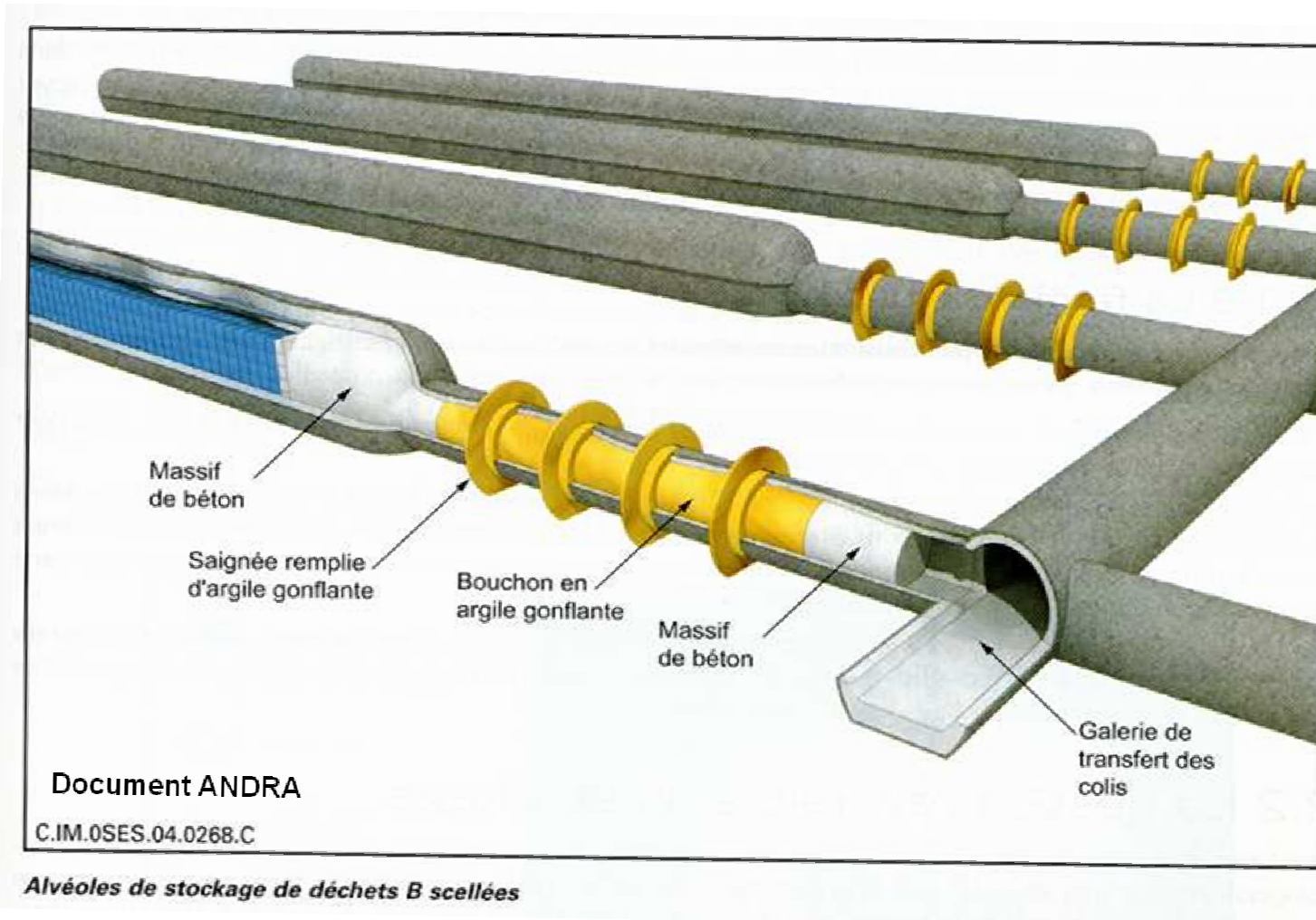
BRGM, Orléans

With the partnership of:

Andra: X. Bourbon, S. Dewonck, I. Munier, N. Michau



CONTEXT: COX/CONCRETE/BENTONITE INTERACTION

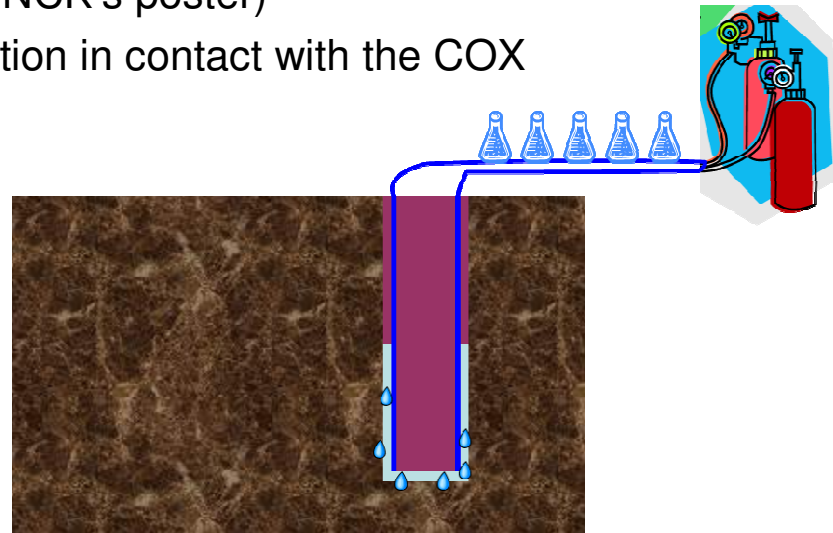
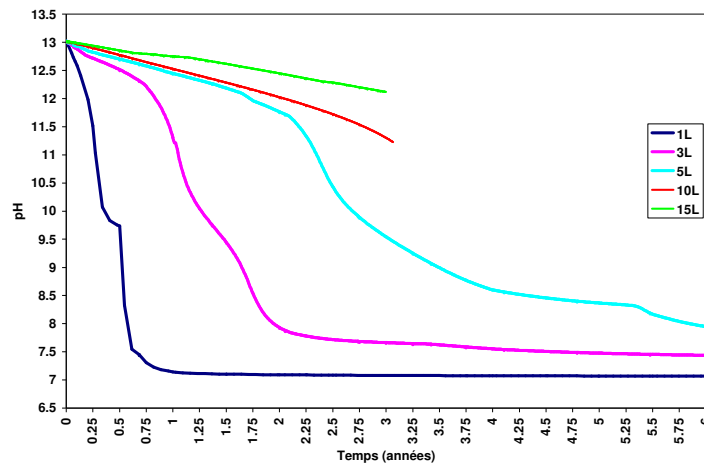


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MODELLING AS A TOOL

> To size a future underground experiment in the Bure's Laboratory

- MLH experiment (see S.DEWONCK's poster)
- pH evolution of an alkaline solution in contact with the COX



> To make some predictive calculations

- Long term modelling of concrete/clay interactions for PA purposes

CRITICAL ELEMENTS FOR THE MODELLING

- > **A coherent thermodynamic database to work in temperature**
- > **A “complete” mineralogical description of the initial system**
- > **Transport parameters (porosities, permeabilities, diffusion coefficients, heat conductivities...)**

- > **A Transport reactive code**
 - PHREEQC (1D)
 - TOUGHREACT (radial geometry, non saturated condition,)
- > **Experiments to test and improve the modelling**
- >

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http://thermoddem.brgm.fr/


Thermoddem - Mozilla Firefox

Fichier Édition Affichage Historique Marque-pages Outils ?

http://thermoddem.brgm.fr/fiche.asp

Les plus visités Club Internet Hotmail Mon Assistance Mon compte Personnaliser les liens http://www.skitour.fr... Windows Media Accès web saturé : po... Page d'accueil de Mozi... Page d'accueil de Mozi...

  **THERMODDEM**
Thermodynamics database devoted to
the modelling of waste minerals alteration

 **Mineral** [Export file \(text format\)](#)

Introduction
Links and addresses
Rights of user
Data consultation

Help
Home page
Login
More info...

Nomenclature
Name of mineral : Foshagite
Formula : $\text{Ca}_4\text{Si}_3\text{O}_9(\text{OH})_2 \cdot 0.5\text{H}_2\text{O}$
family : Inosilicates, Wollastonite-2M - Foshagite series

Other members :
Hillebrandite ($\text{Ca}_2\text{SiO}_3(\text{OH})_2 \cdot 0.17\text{H}_2\text{O}$)
Wollastonite (CaSiO_3)

Polymorphs : No polymorph...

Mineralogy
Space group : Monoclinic - Prismatic H-M Symbol (2/m) Space Group: P 21/m
Dana class : 65.2.2.1 (65) Inosilicate Single-Width Unbranched Chains, W=1(65.2) with chains P=3 (65.2.2) Dana Group

Occurrence & geological context
Metamorphosed limestone.

Alteration & pathway
Confined medium :
Weathering :

Thermodynamics
Properties of formation from the elements
 ΔG_f° : -5 643 832 J/mol [Ref.](#) [Info](#) Mol wt: 431.5870 g/mol
 ΔH_f° : -6 032 430 J/mol [Ref.](#) [Info](#) V : 160.6600 cm^3/mol [Ref.](#) [Info](#)
S°: 295.07 J/mol K [Ref.](#) [Info](#)

Test (consistency): 2 D [Cp Information](#)

Reaction properties $\text{Ca}_4\text{Si}_3\text{O}_9(\text{OH})_2 \cdot 0.5\text{H}_2\text{O} + 8\text{H}^+ + 0.5\text{H}_2\text{O} = 4\text{Ca}^{++} + 3\text{H}_4\text{SiO}_4$

Van t'Hoff
Log K: 65.96 [Ref.](#) [Info](#) ΔH_f° : -380 238 J/mol [Ref.](#) [Info](#)

Analytic
 $\text{Log K} = A + BT + CT^{-1} + D \text{Log}T + ET^{-2}$
A : -1 116.01
B : -0.17
C : 78 338.50
D : 405.82

T (°C)	0	25	60	100
	150	200	250	300
	72.08	65.96	59.01	52.75

Terminé

AMORPHOUS CSH

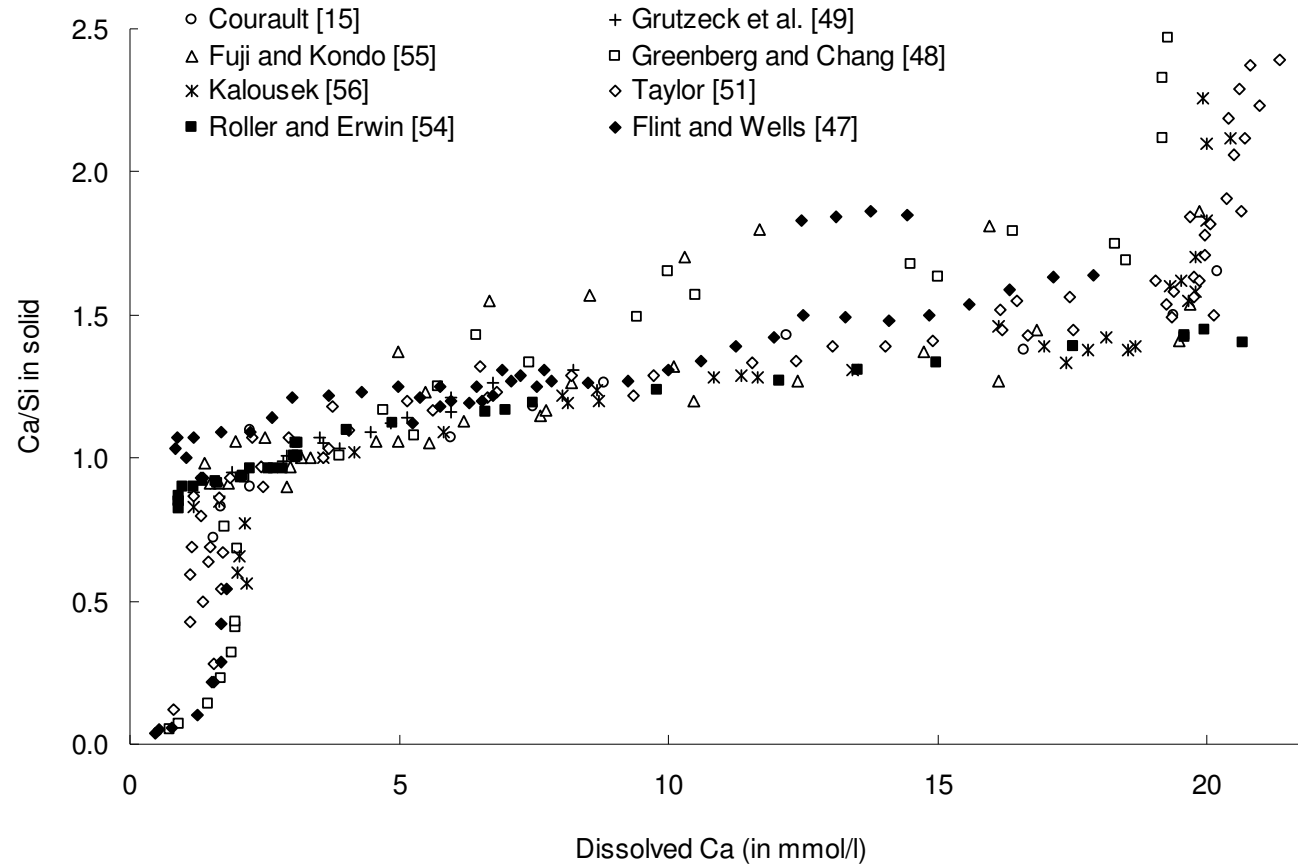
- > Among the various models published that take into account the solubility of CSH, two main families may be distinguished:**
 - Discrete phases
 - Solid solutions

- > Nowadays integration of solid solutions in transport geochemical codes lead to crippling computing times**

COMPOSITION OF AMORPHOUS CSH PHASES (1/4)

- > According to the literature and given the crystallographic constraints a 3-phases model was chosen**
- > Such model already exist (CSH0.8/1.1/1.8)**
 - Stronach and Glasser (1997) Adv. Cem. Res. Vol. 36 pp.167
 - A.C. Courault (2000) Thesis Université de Bourgogne
- > Strategy used : fitting of the literatures data with a least squares algorithm**

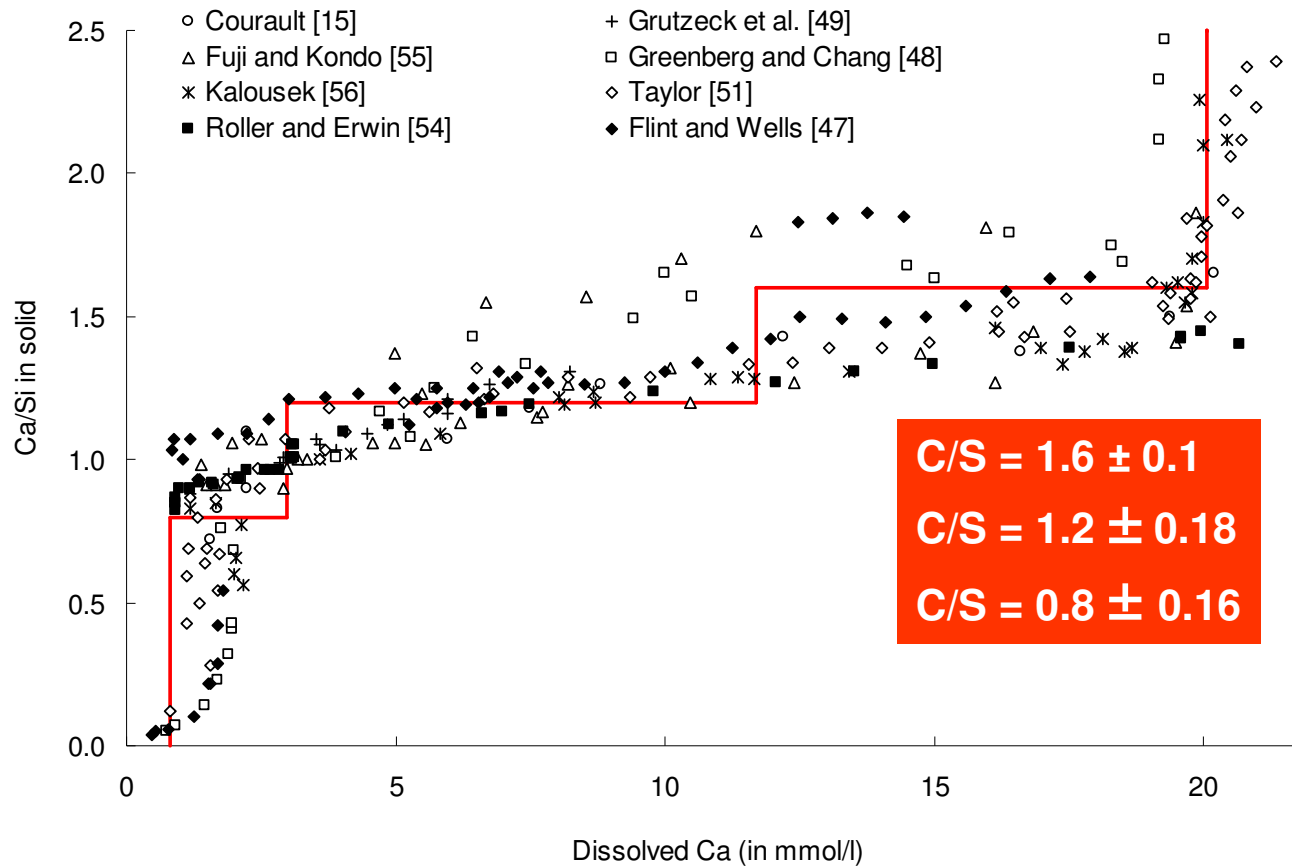
COMPOSITION OF AMORPHOUS CSH PHASES (2/4)



Dispersion in the values can be link to :

- ✓ The synthesis route followed
- ✓ The pathway followed to reach equilibrium (by dissolution or precipitation)
- ✓ The assessment of the C/S ratio in the solid
- ✓ A solid/liquid equilibrium not reached due to kinetic constraints

COMPOSITION OF AMORPHOUS CSH PHASES (3/4)

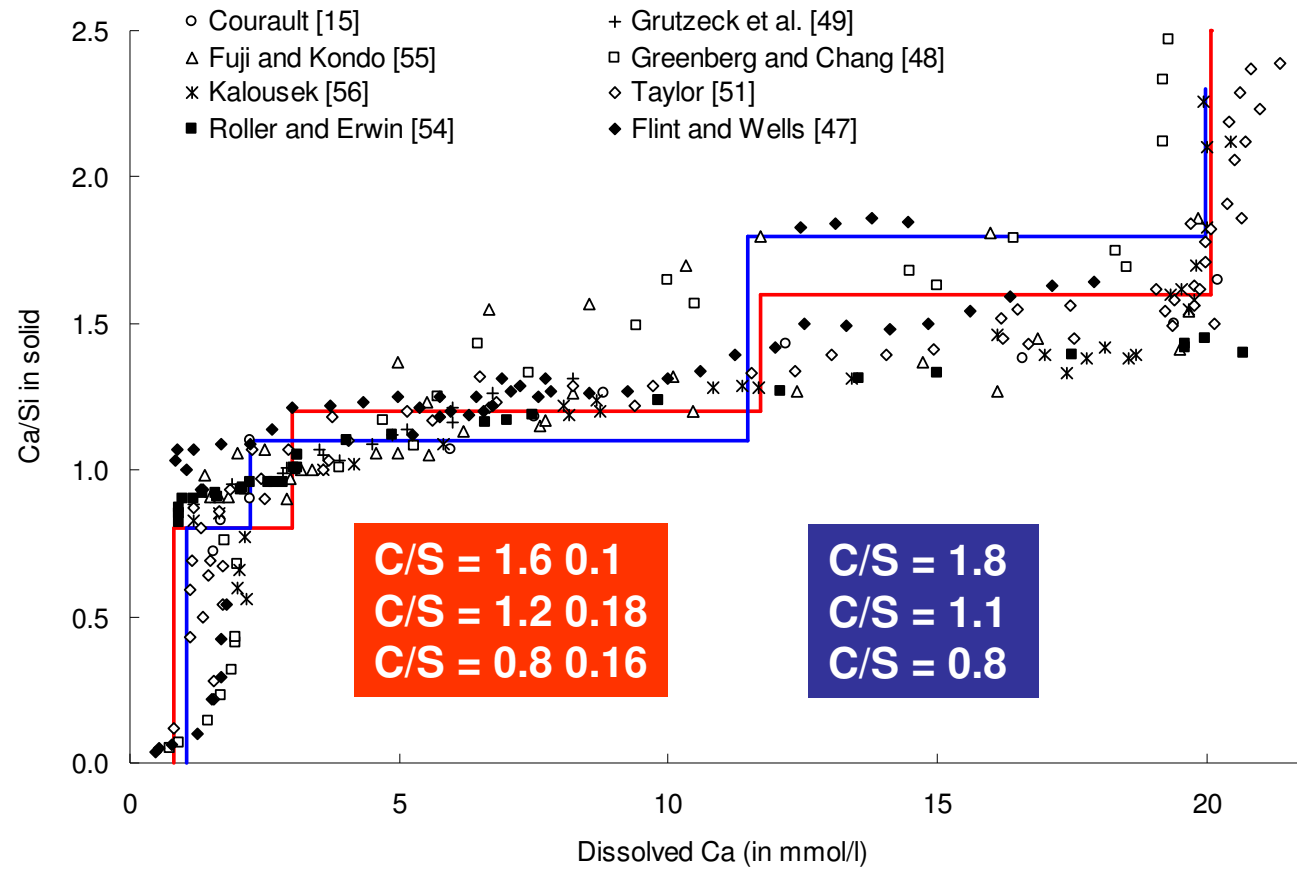


Blanc, P. et al. accepted. Chemical conceptual model for cement-based materials: Thermodynamic data assessment of stoichiometric and non-stoichiometric CSH phases. *J.Hazardous.Materials*

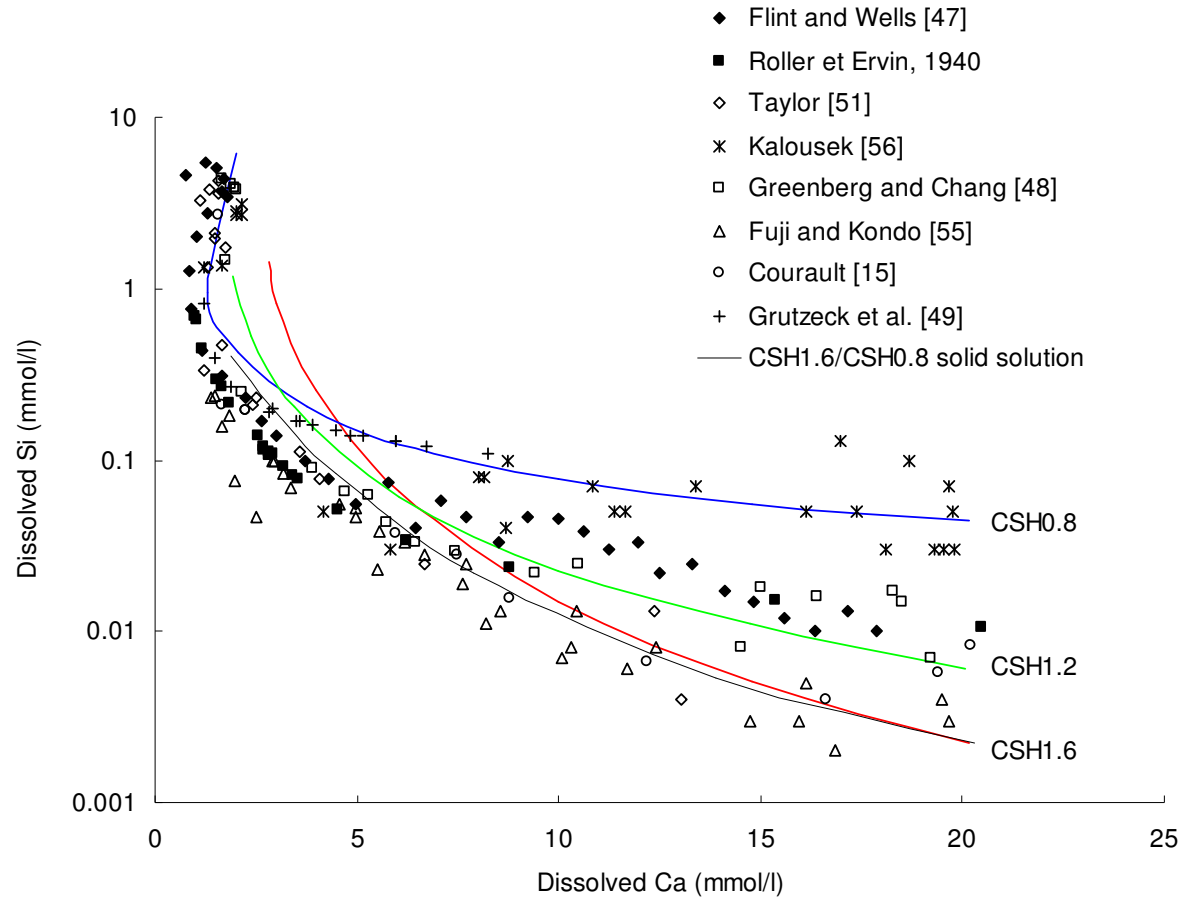
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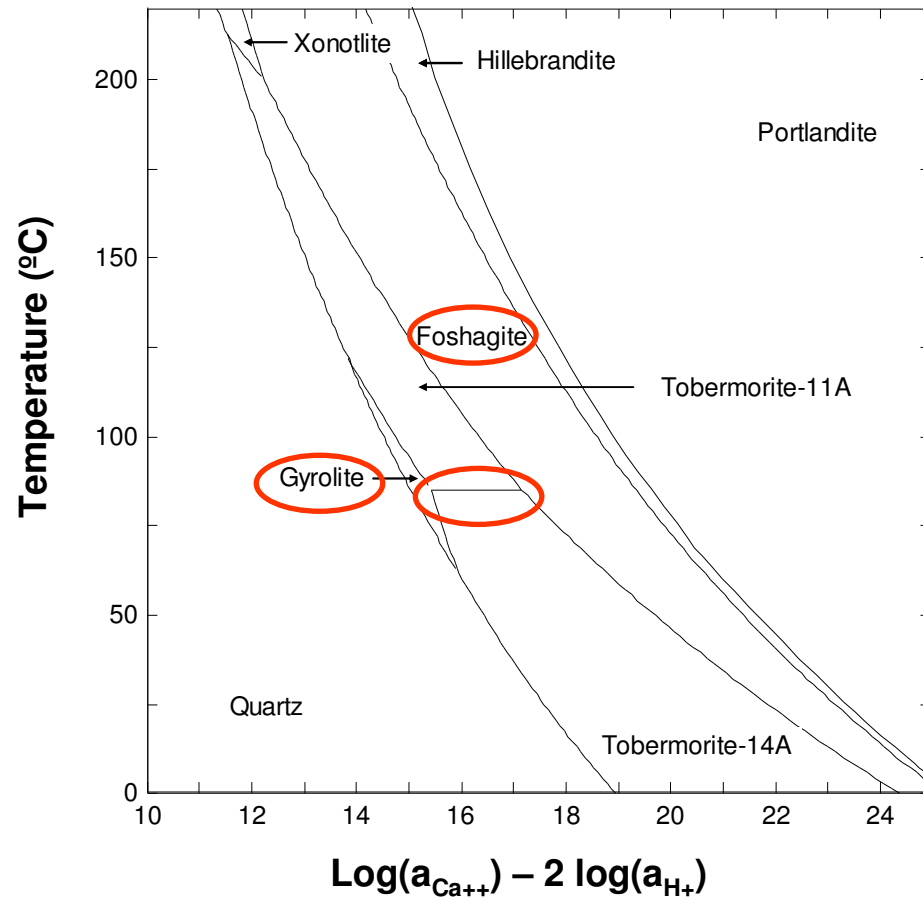
COMPOSITION OF AMORPHOUS CSH PHASES (3/4)



COMPOSITION OF AMORPHOUS CSH PHASES (4/4)



CRYSTALLINE CSH PHASES (1/2)

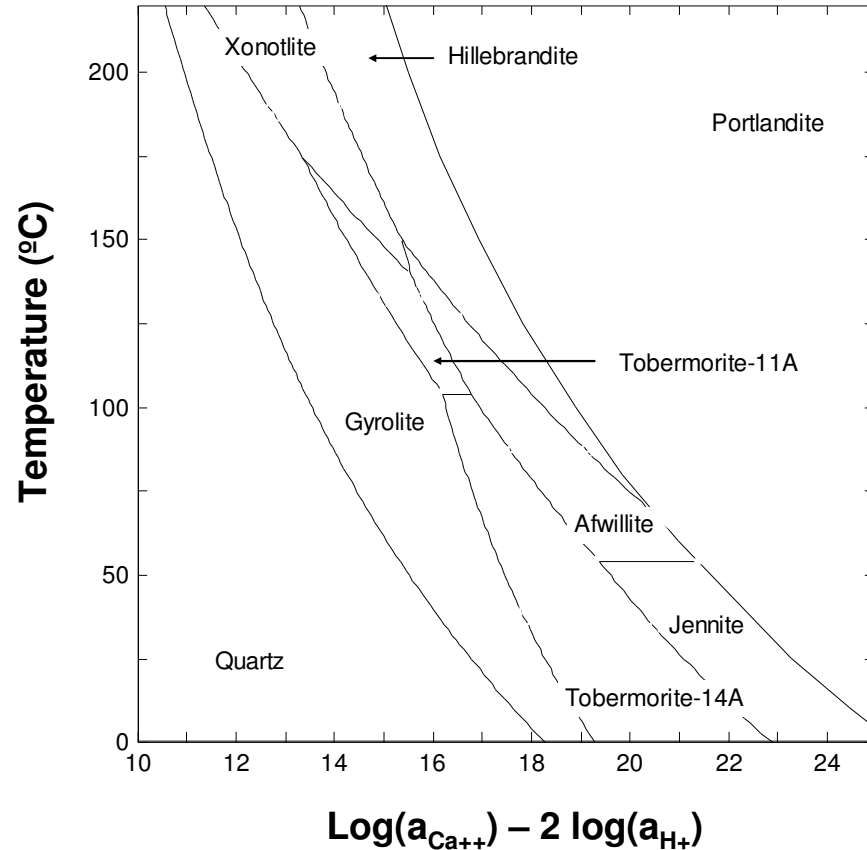


- ✓ Temperature transition to low
- ✓ Authors see this phase at least up to 200 °C
- ✓ Foshagite considered as high temperature phase
- ✓ Absence of okenite, afwillite and jennite

Diagram calculated using the estimates of Babushkin et al. (EQ3.6)

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CRYSTALLINE CSH PHASES (2/2)



Hypotheses :

- ✓ Use of triple point (Gibbs phases rule)
- ✓ ΔH of Tobermorite 11A°, Xonotlite, Foshagite and Hillebrandite are fixed
- ✓ The C_p of Babushkin were used

Phases	Température d'équilibre (°C)	Référence
AFW + POR + HIL	100 (100)	Hong et Glasser, 2004 Heller et Taylor, 1952
AFW + FOS + HIL	170 (169)	Hong et Glasser, 2004
AFW + XON + Hill	150 (150)	D'après Hong et Glasser, 2004 ; Atkinson et al., 1995
TOB11 + AFW + XON	140 (140)	El-Hemaly et al., 1977
TOB11 + TOB14	105 (104)	Maeshimae et al., 2003
TOB11 + XON + GYR	175 (174)	Kalousek et Nelson, 1978
JEN + Afwillite	T < 55°C (55)	Atkins et al., 1994
Tobermorite-14A, $\text{Log}K_{85^\circ\text{C}} = 54.25$ (54.25)		Atkinson et al., 1994
Jennite : $147.10 < \text{Log}K_{25^\circ\text{C}} < 150.81$ (147.33)		Revertgat et al., 1997

Blanc, P. et al. accepted.
J. Hazardous Materials

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STARTING MINERALOGICAL CONDITIONS (CONCRETE)

Amorphous hypothesis @ 25°C (1)

Mineral	Structural formula	Volume fraction	Concentration mol/L
C3FH6	$\text{Ca}_3\text{Fe}_2(\text{OH})_{12}$	0.0216	0.94
Calcite	CaCO_3	0.7225	130.68
→ CSH1.6	$\text{Ca}_{1.6}\text{SiO}_{3.6}(\text{H}_2\text{O})_{2.58}$	0.1373	10.83
Ettringite	$\text{Ca}_6\text{Al}_2(\text{SO}_4)_3(\text{OH})_{12}(\text{H}_2\text{O})_{26}$	0.0381	0.36
Hydrotalcite	$\text{Mg}_4\text{Al}_2\text{O}_7(\text{H}_2\text{O})_{10}$	0.0041	0.12
→ KatoiteSi	$\text{Ca}_3\text{Al}_2(\text{SiO}_4)(\text{OH})_8$	0.0135	0.64
Portlandite	$\text{Ca}(\text{OH})_2$	0.0629	12.72

Cristalline hypothesis @ 25°C (2)

Mineral	Structural formula	Volume fraction	Concentration mol/L
→ C3AH6	$\text{Ca}_3\text{Al}_2(\text{OH})_{12}$	0.0144	0.66
C3FH6	$\text{Ca}_3\text{Fe}_2(\text{OH})_{12}$	0.0216	0.96
Calcite	CaCO_3	0.7154	130.15
Ettringite	$\text{Ca}_6\text{Al}_2(\text{SO}_4)_3(\text{OH})_{12}(\text{H}_2\text{O})_{26}$	0.0396	0.37
Hydrotalcite	$\text{Mg}_4\text{Al}_2\text{O}_7(\text{H}_2\text{O})_{10}$	0.0042	0.12
→ Jennite	$\text{Ca}_9\text{Si}_6\text{H}_{22}\text{O}_{32}$	0.1329	1.97
Portlandite	$\text{Ca}(\text{OH})_2$	0.0729	13.24

Hyp1 Hyp2

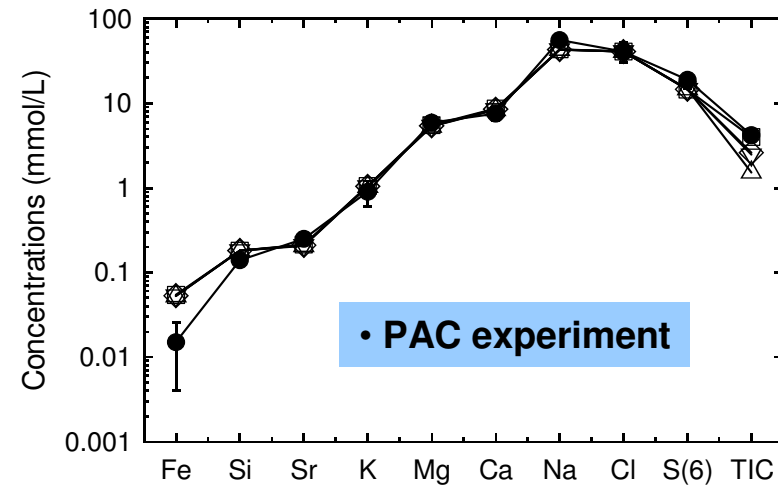
Element	Concentration mmol/L	
Al	$2.3 \cdot 10^{-2}$	$4.93 \cdot 10^{-2}$
C	$7.46 \cdot 10^{-3}$	$4.46 \cdot 10^{-3}$
Ca	$2.02 \cdot 10^1$	$2.02 \cdot 10^1$
Cl	$4.10 \cdot 10^1$	$4.10 \cdot 10^1$
Fe	$6.05 \cdot 10^{-5}$	$1.25 \cdot 10^{-4}$
K	$8.35 \cdot 10^{-1}$	$8.35 \cdot 10^{-1}$
Mg	$4.56 \cdot 10^{-6}$	$3.11 \cdot 10^{-6}$
Na	$4.58 \cdot 10^1$	$4.58 \cdot 10^1$
S	$2.08 \cdot 10^{-2}$	$1.85 \cdot 10^{-2}$
Si	$2.49 \cdot 10^{-3}$	$1.70 \cdot 10^{-4}$
Sr	$2.01 \cdot 10^{-1}$	$2.01 \cdot 10^{-1}$
pH	12.5	

Pore water composition after resaturation with COX pore water

CEM I + calcite aggregate

STARTING MINERALOGICAL CONDITIONS (COX)

Mineral	Structural formula	Volume fraction	mol/L	Element	Concentration (mmol/KgW)
Calcite	CaCO ₃	0.2262	27.89	Al	6.93 10 ⁻⁶
Celestite	SrSO ₄	0.0067	0.66	Fe	4.84 10 ⁻²
Chlorite	Fe ₅ Al(AlSi ₃)O ₁₀ (OH) ₈	0.0167	0.36	Si	0.18
Dolomite	CaMg(CO ₃) ₂	0.0408	2.90	Sr	0.21
Illite	K _{0.85} Mg _{0.25} Al _{2.35} Si _{3.4} O ₁₀ (OH) ₂	0.3406	10.74	K	0.83
Feldspath K	K(AlSi ₃)O ₈	0.0312	1.31	Mg	5.58
Smectite	Ca _{0.01} Na _{0.434} K _{0.026} (Si _{3.612} Al _{0.388})Al _{1.608} Fe _{0.222} Mg _{0.228} O ₁₀ (OH) ₂ ·5.441H ₂ O	0.0765	2.62	Ca	8.80
Pyrite	FeS ₂	0.0053	1.01	Na	45.80
Quartz	SiO ₂	0.2465	49.50	Cl	41.00
Siderite	FeCO ₃	0.0095	1.47	S(6)	16.30
Porosity	0.18			TIC	2.53
				pH	7.21



Gaucher et al. Submitted to GCA

STARTING MINERALOGICAL CONDITIONS (MX80 bentonite)

Mineral	Structural formula	Volume Fraction	mol/L	Element	Concentration (mmol/KgW)
Plagioclase	$\text{NaAlSi}_3\text{O}_8$	0.0683	1.27	Al	$4.43 \cdot 10^{-5}$
Calcite	CaCO_3	0.0061	0.31	Ca	$6.25 \cdot 10^{-2}$
Dolomite	$\text{CaMg}(\text{CO}_3)_2$	0.0000	0.00	Cl	$4.01 \cdot 10^1$
Feldspath K	$\text{K}(\text{AlSi}_3)\text{O}_8$	0.0151	0.26	Fe	$8.43 \cdot 10^{-3}$
Smectite	$\text{Ca}_{0.01}\text{Na}_{0.434}\text{K}_{0.026}(\text{Si}_{3.612}\text{Al}_{0.388})\text{Al}_{1.608}\text{Fe}_{0.222}\text{Mg}_{0.228}\text{O}_{10}(\text{OH})_2 \cdot 5.441\text{H}_2\text{O}$	0.5454	7.55	K	$3.46 \cdot 10^{-1}$
Pyrite	FeS_2	0.0197	0.17	Mg	$3.78 \cdot 10^{-2}$
Quartz	SiO_2	0.3327	27.23	Na	$1.01 \cdot 10^2$
Siderite	FeCO_3	0.0028	0.18	S	$1.64 \cdot 10^1$
Porosity	0.35			Si	$1.92 \cdot 10^{-1}$
				Sr	$9.72 \cdot 10^{-4}$
				TIC	$2.66 \cdot 10^1$
				pH	8.40

70% MX80 + 30% Sand

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TRANSPORT PARAMETERS

Material	Effective diffusion coefficient (m ² .s ⁻¹)	Porosity	Poral diffusion coefficient (m ² .s ⁻¹)
Concrete (amorphe)	9.0 10 ⁻¹²	0.135	6.67 10 ⁻¹¹
Concrete (cristalline)	9.0 10 ⁻¹²	0.135	6.67 10 ⁻¹¹
Bentonite (MX80)	1.0 10 ⁻¹¹	0.37	2.70 10 ⁻¹¹
COX	1.0 10 ⁻¹¹	0.18	5.56 10 ⁻¹¹

$$D_{0,T} = D_{0,298} \cdot \frac{T}{298} \cdot \frac{\eta_{298}}{\eta_T}$$

$$\eta_T = \exp \left(\ln 10 \cdot (-1.37023 \cdot (tc - 20) + \frac{8.36 \cdot 10^{-4} \cdot (tc - 20)^2}{109 + tc}) \right)$$

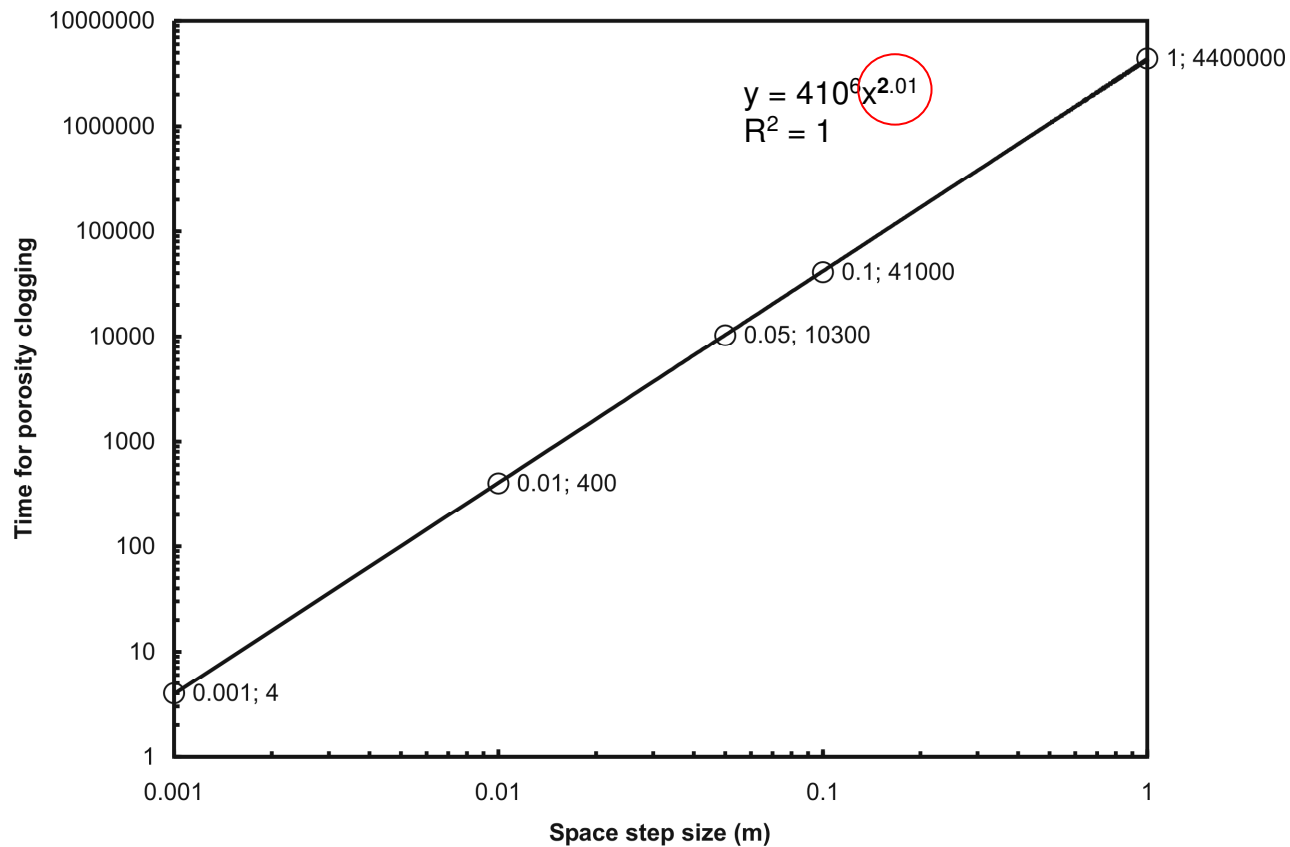
Ratio 2.54 between 70°C and 25°C

1D cartesian saturated conditions: PHREEQC

1D radial non-saturated conditions: TOUGHREACT

- ✓ The release of the MCD option in PHREEQC permits to treat multi-porosity cases
- ✓ However, MCD option still under improvement : => use of Mix Cells instead
cf. Appelo et al. (2008) Journal of Contaminant Hydrology Vol 101 pp 67

INFLUENCE OF MESH SIZE (at local equilibrium)

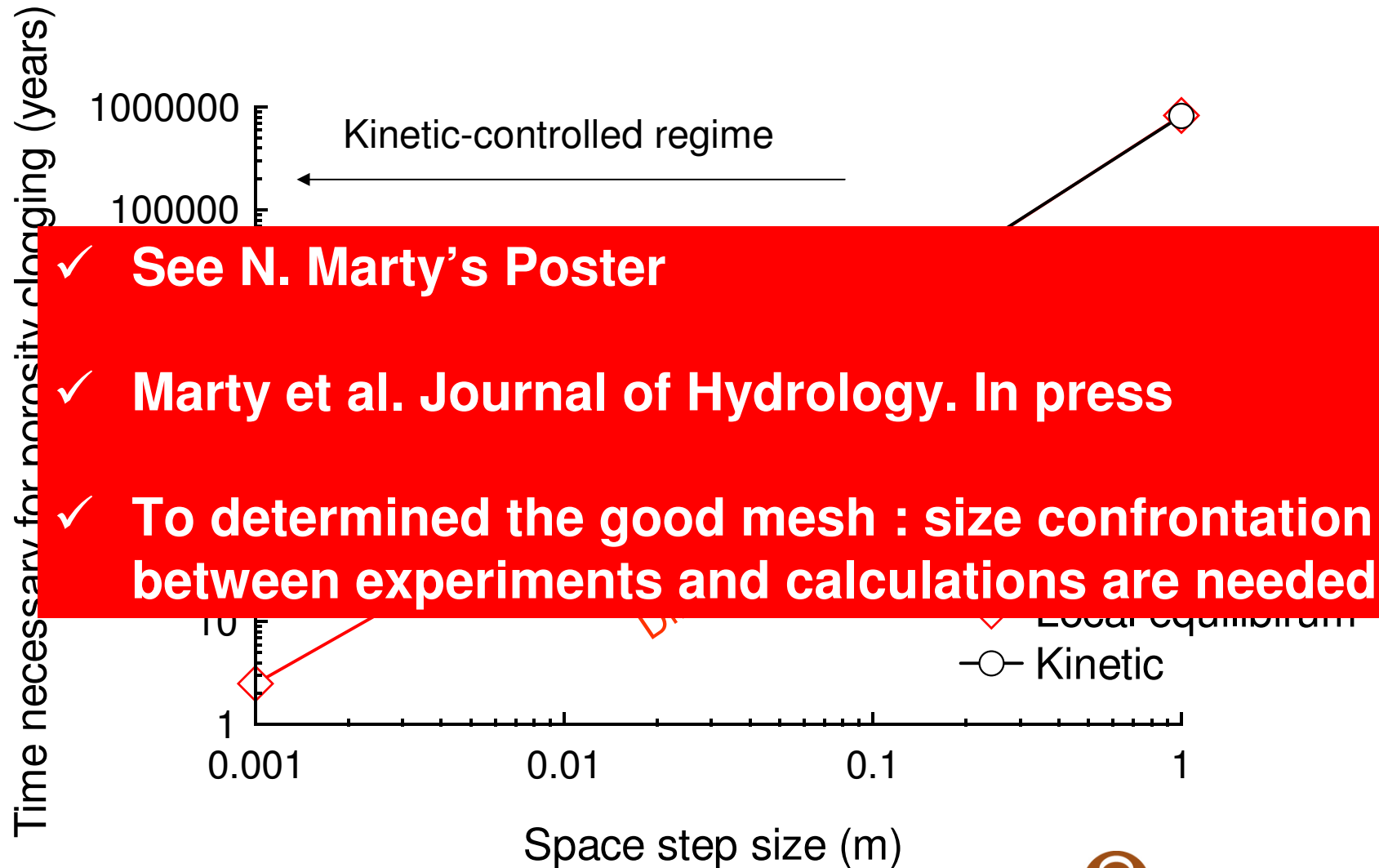


Diffusion controlled :

$$x^2 = Dt$$

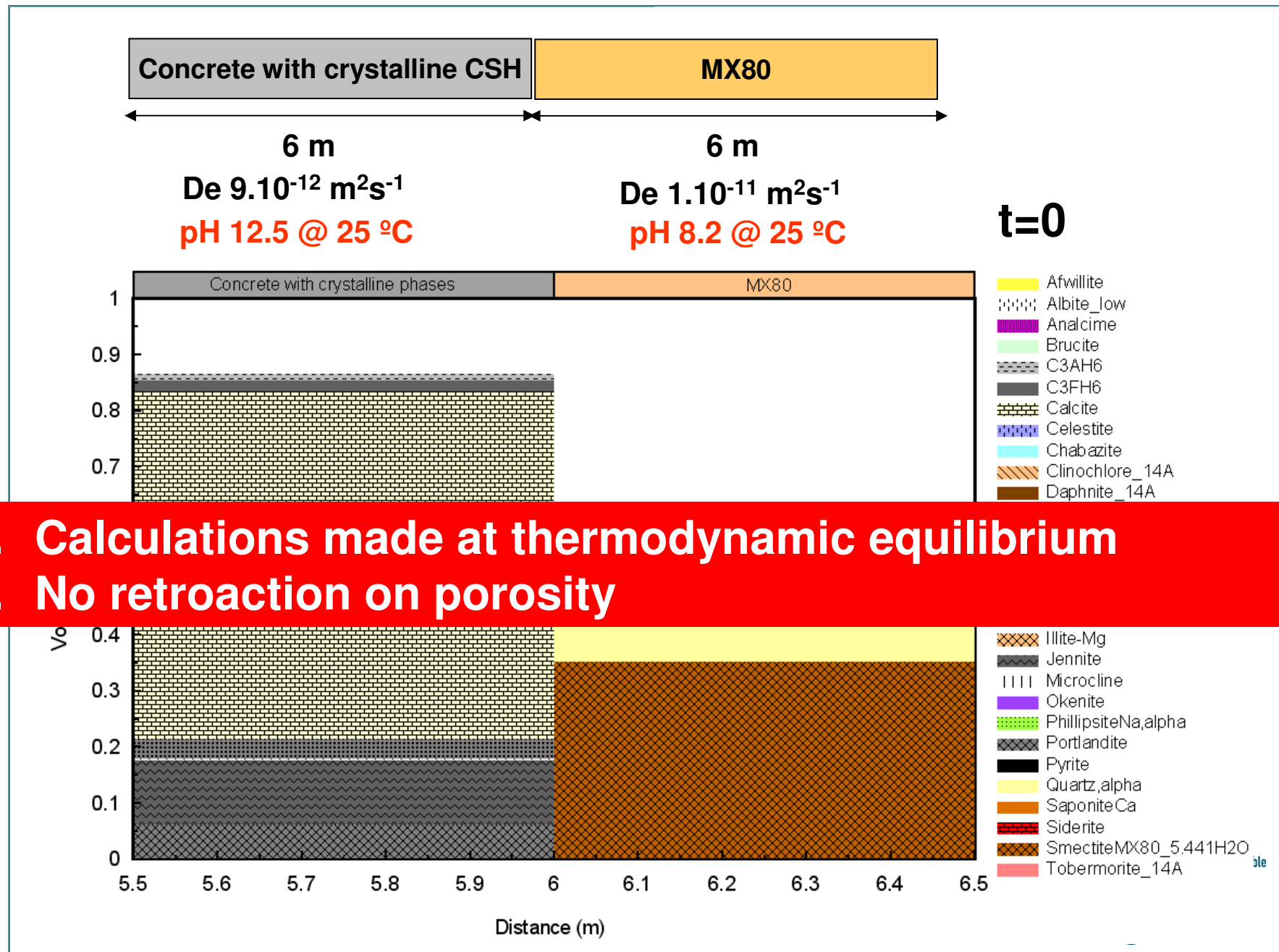
$$2 \log x = \log D + \log t$$

INFLUENCE OF MESH SIZE



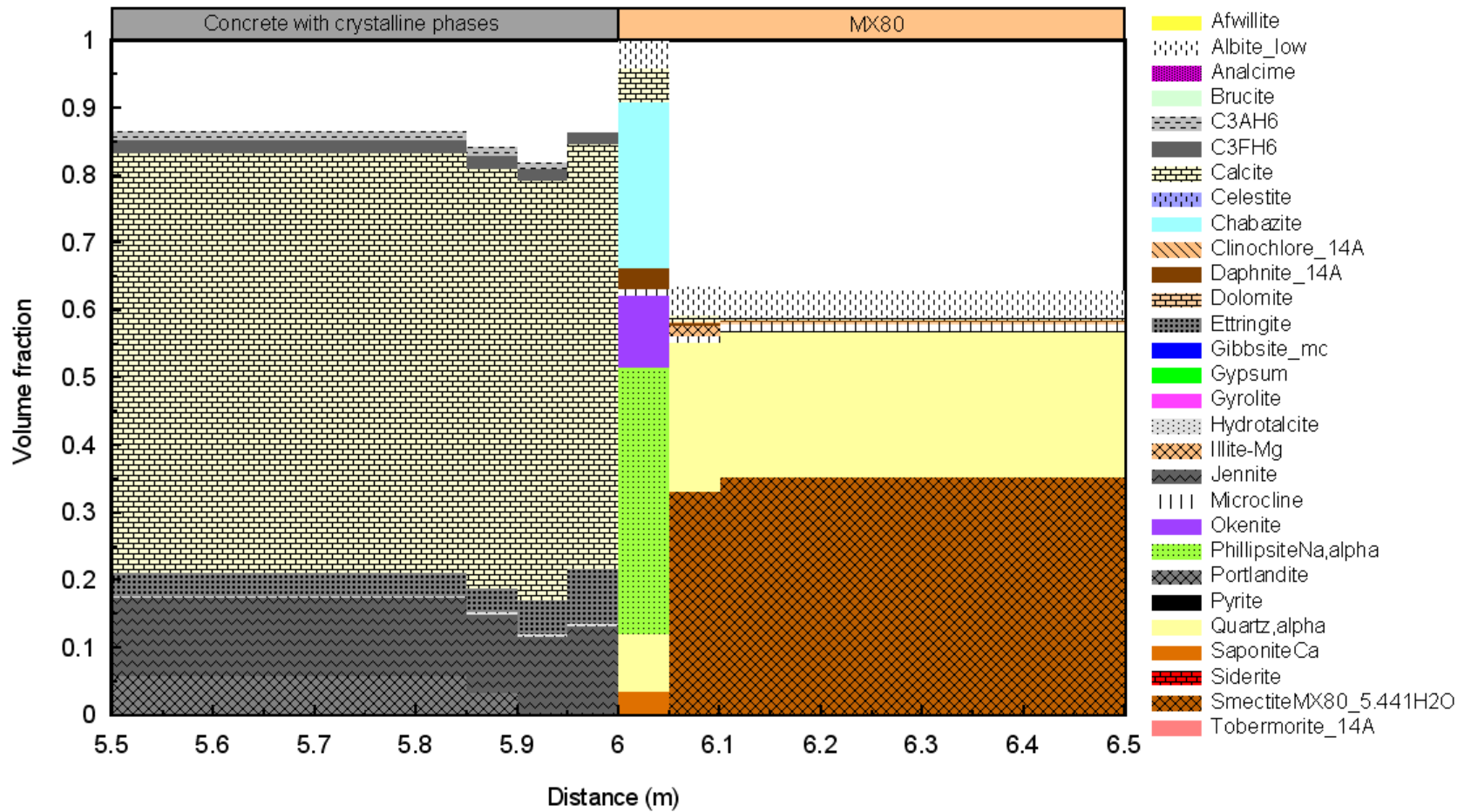
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1. Calculations made at thermodynamic equilibrium
2. No retroaction on porosity

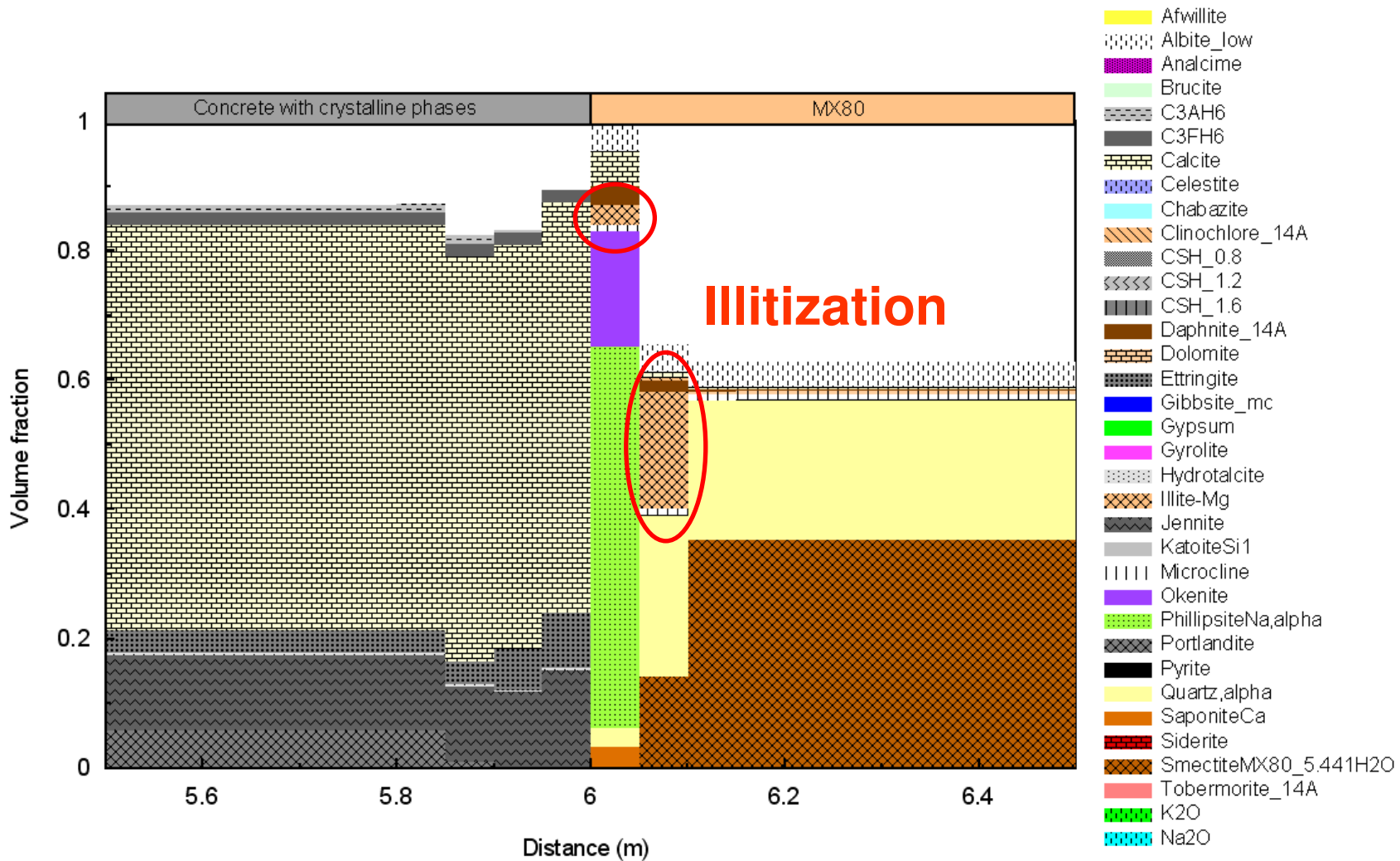
Time for porosity clogging = 2700 years



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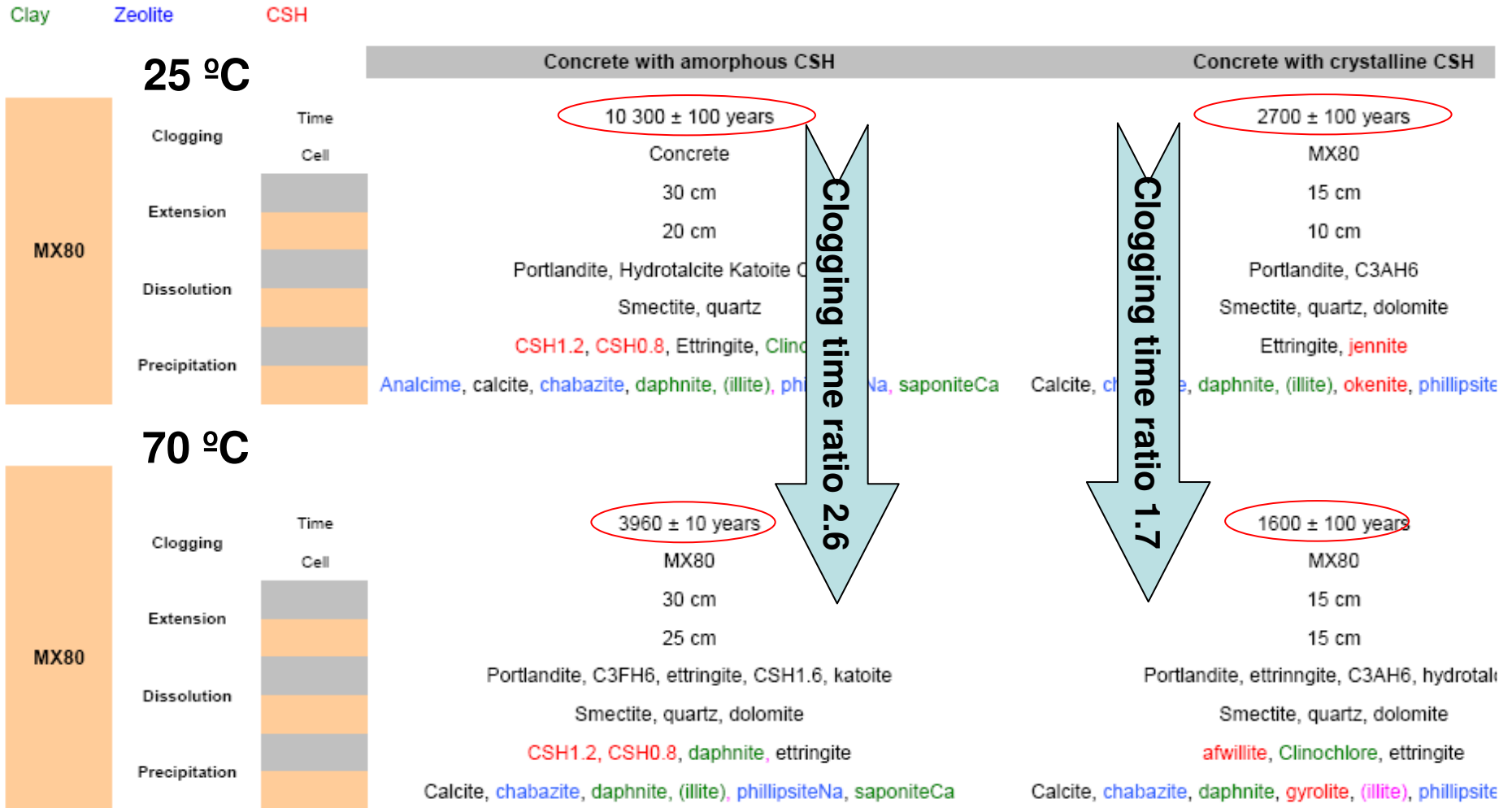
« Young » concrete pH13.2 Time for porosity clogging 3500 ans

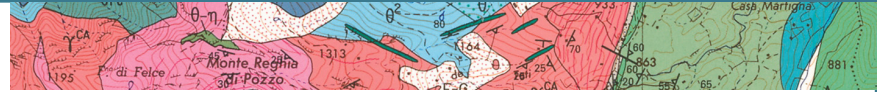


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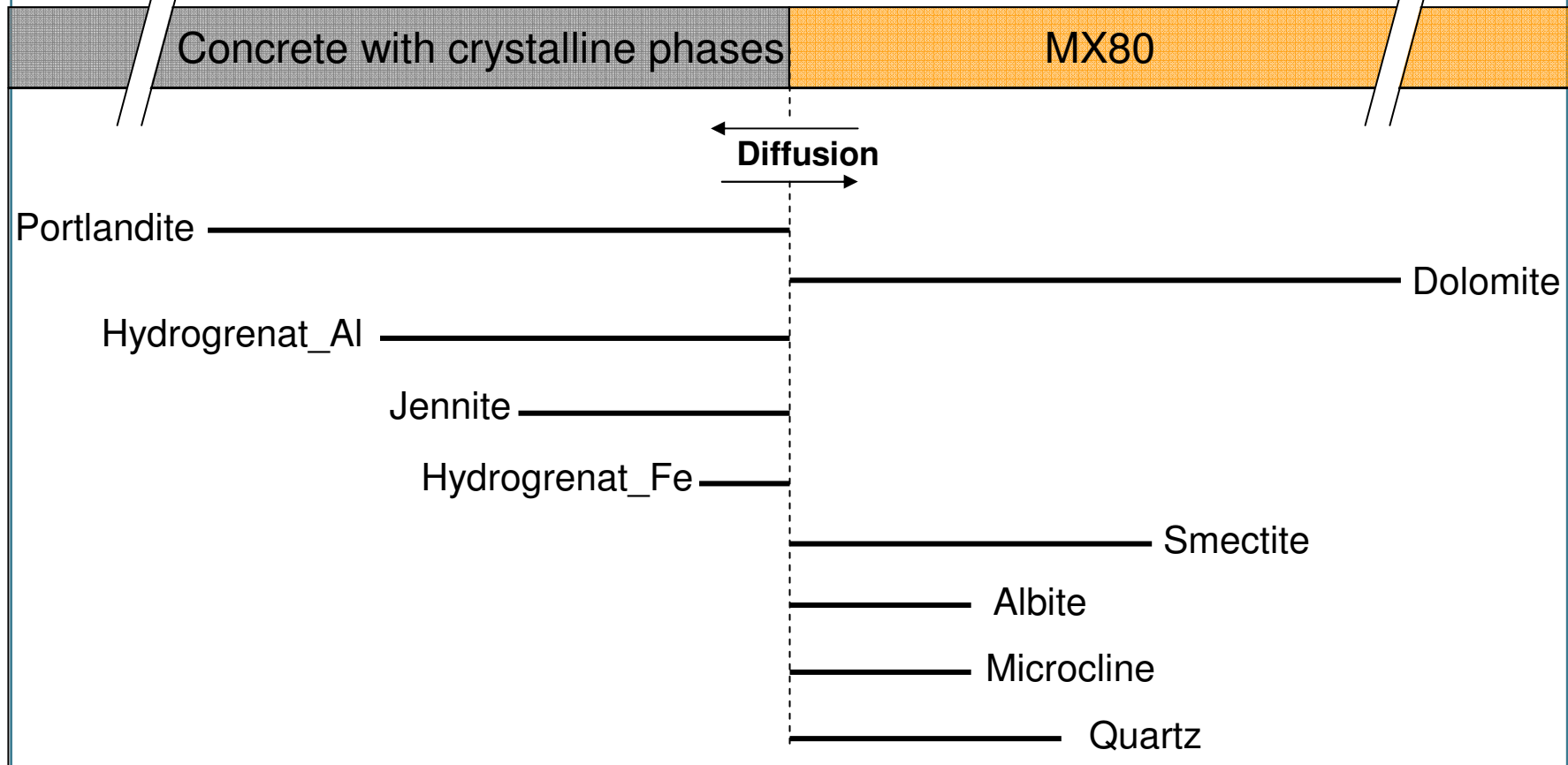


TEMPERATURE INFLUENCE ON CLOGGING





Dissolution sequence of primary phases

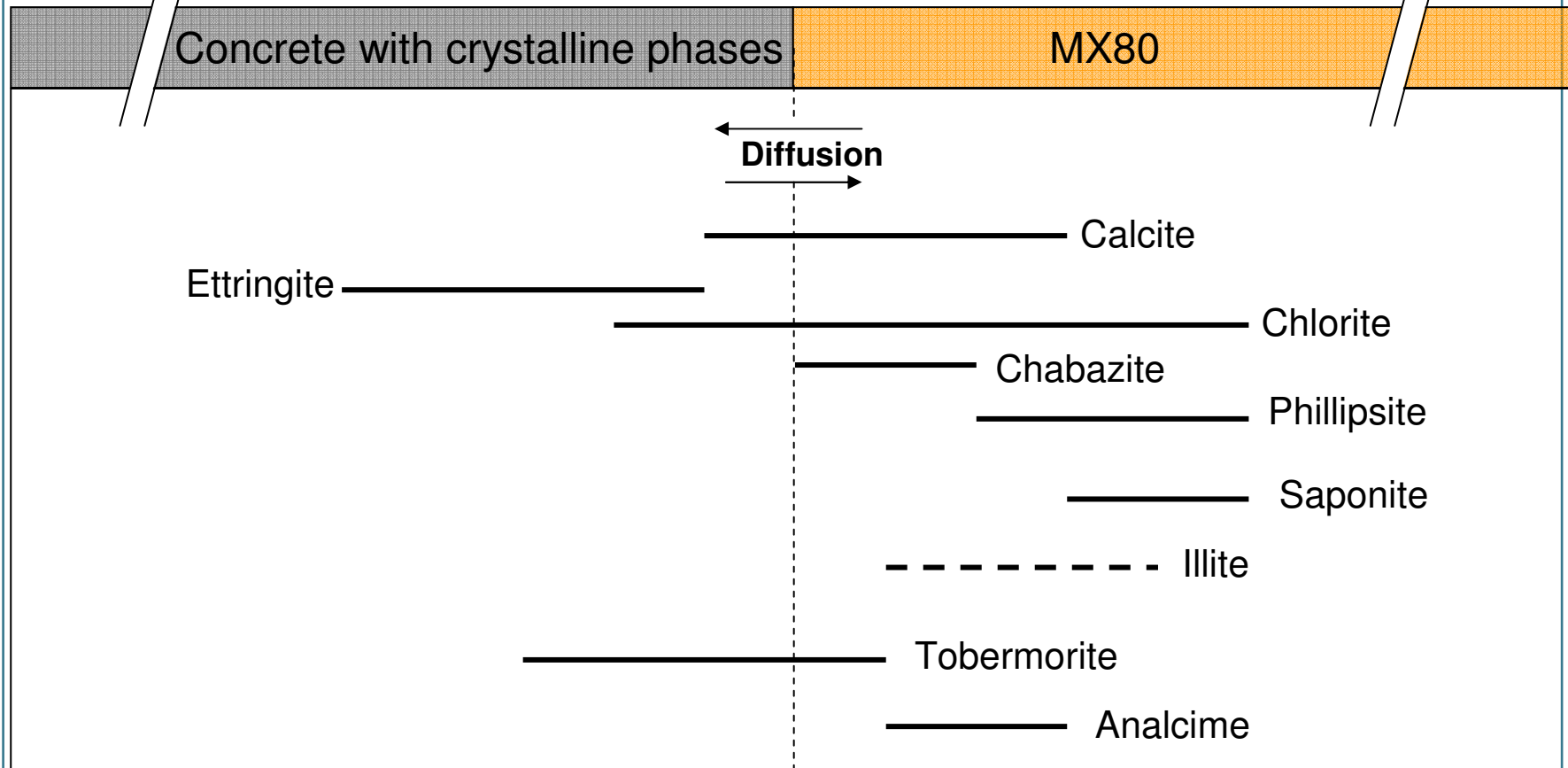


← Altered zone: less than 50 cm
at the clogging time





Precipitation sequence of secondary phases



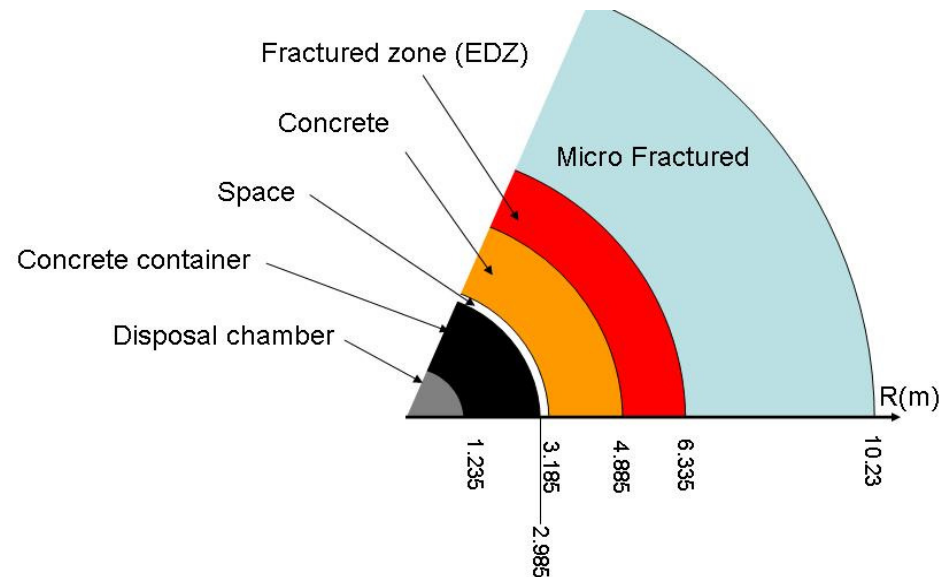
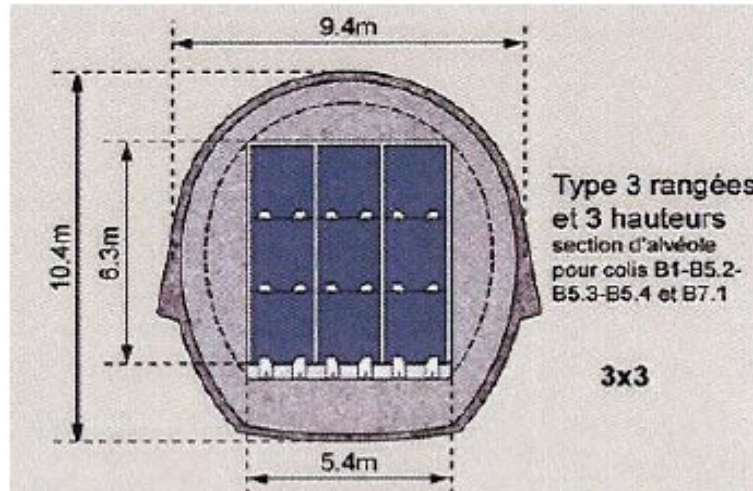
← Altered zone: less than 50 cm at the clogging time



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TOWARD A MORE REALISTIC GEOMETRY



Name	Calculated radius (m)	Chosen radius in the mesh (m)	Difference (%)	Number of mesh
R_{Cp}	1,234	1,235	0,08%	1 of 1.235 m
R_{BC}	2,985	2,985	0,00%	35 of 5 cm
R_{jext}				4 of 5cm
R_{BR}				34 of 5 cm
R_{ZF}				29 of 5 cm
R_{MF}				87 of 5cm
$R_{Cox Sal.}$				60 mesh of variable length

Space :

- Saturated case : concrete porewater
- Non Saturated case : air

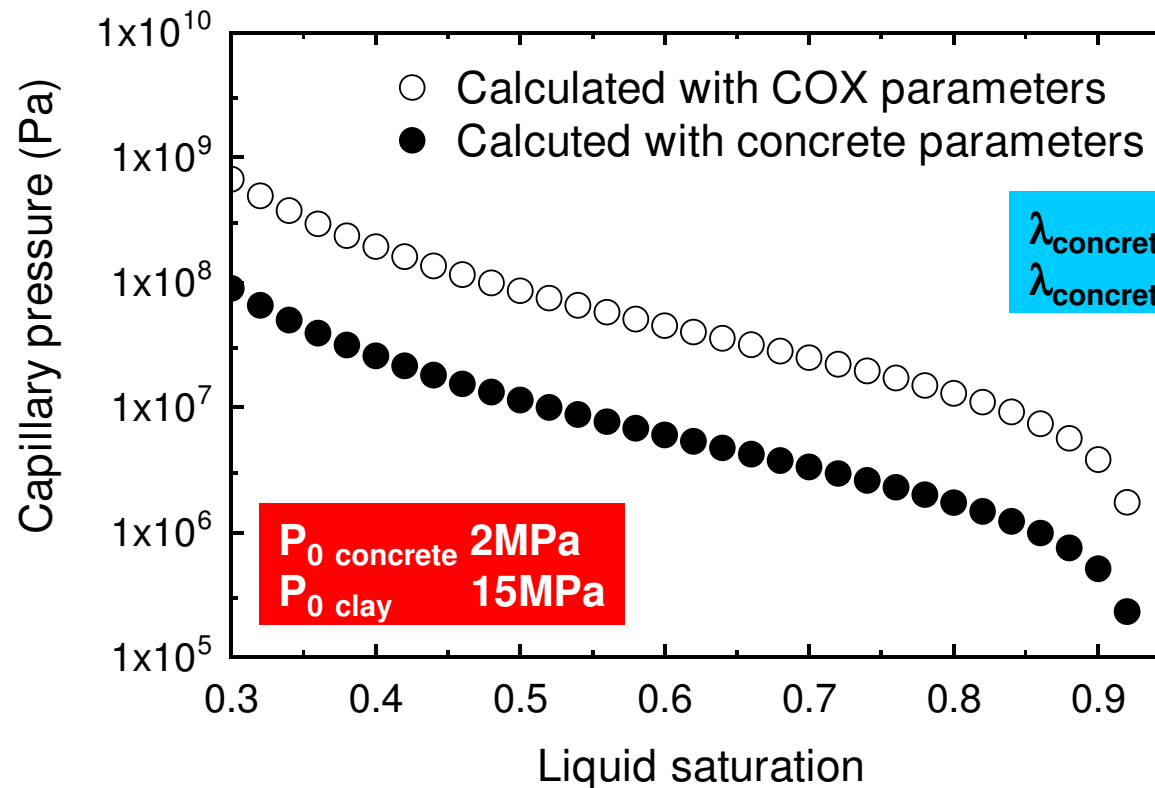
✓ Hypothesis of volume conservation

CAPILLARY PRESSURE FONCTION

NON SATURATED CONDITIONS

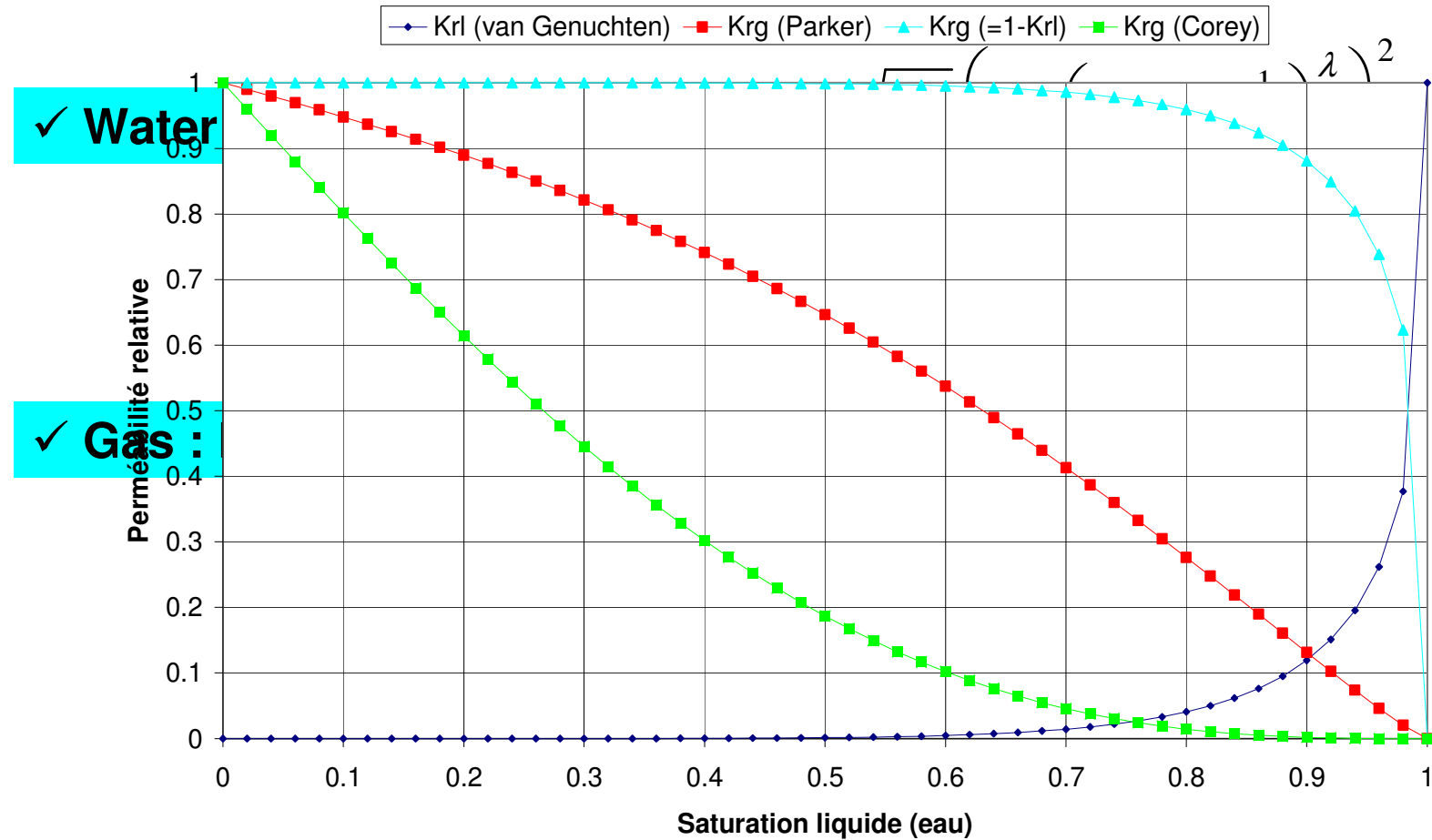
$$P_{cap} = -P_0 \left([S^*]^{\frac{-1}{\lambda}} - 1 \right)^{1-\lambda} \quad S^* = \frac{S_l - S_{lr}}{S_{ls} - S_{lr}}$$

Van Genuchten function

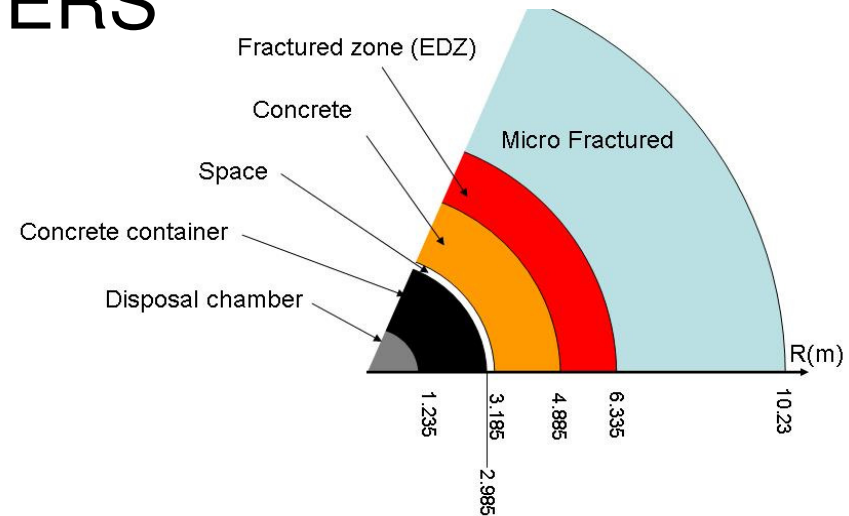


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RELATIVE PERMEABILITY FUNCTION



TRANSPORT PARAMETERS



Material	Permeability K (ms ⁻¹)	Porosity (%)	Effectif diffusion coefficient (m ² s ⁻¹)	
COX	1,6 10 ⁻¹³	18	10 ⁻¹¹	(ANDRA, 2005d)
Microfractured	5,0 10 ⁻¹¹	18	10 ⁻¹¹	(ANDRA, 2005d)
EDZ	5,0 10 ⁻⁹	20	2.10 ⁻¹¹	(ANDRA, 2005d)
Concrete containers	10 ⁻¹¹	13,5	2.10 ⁻¹²	Munier (2008)
Concrete	10 ⁻¹⁰	13,0	9.10 ⁻¹²	Munier (2008)
Space	1,0 10 ⁻⁸	100	2.10 ⁻⁰⁹	

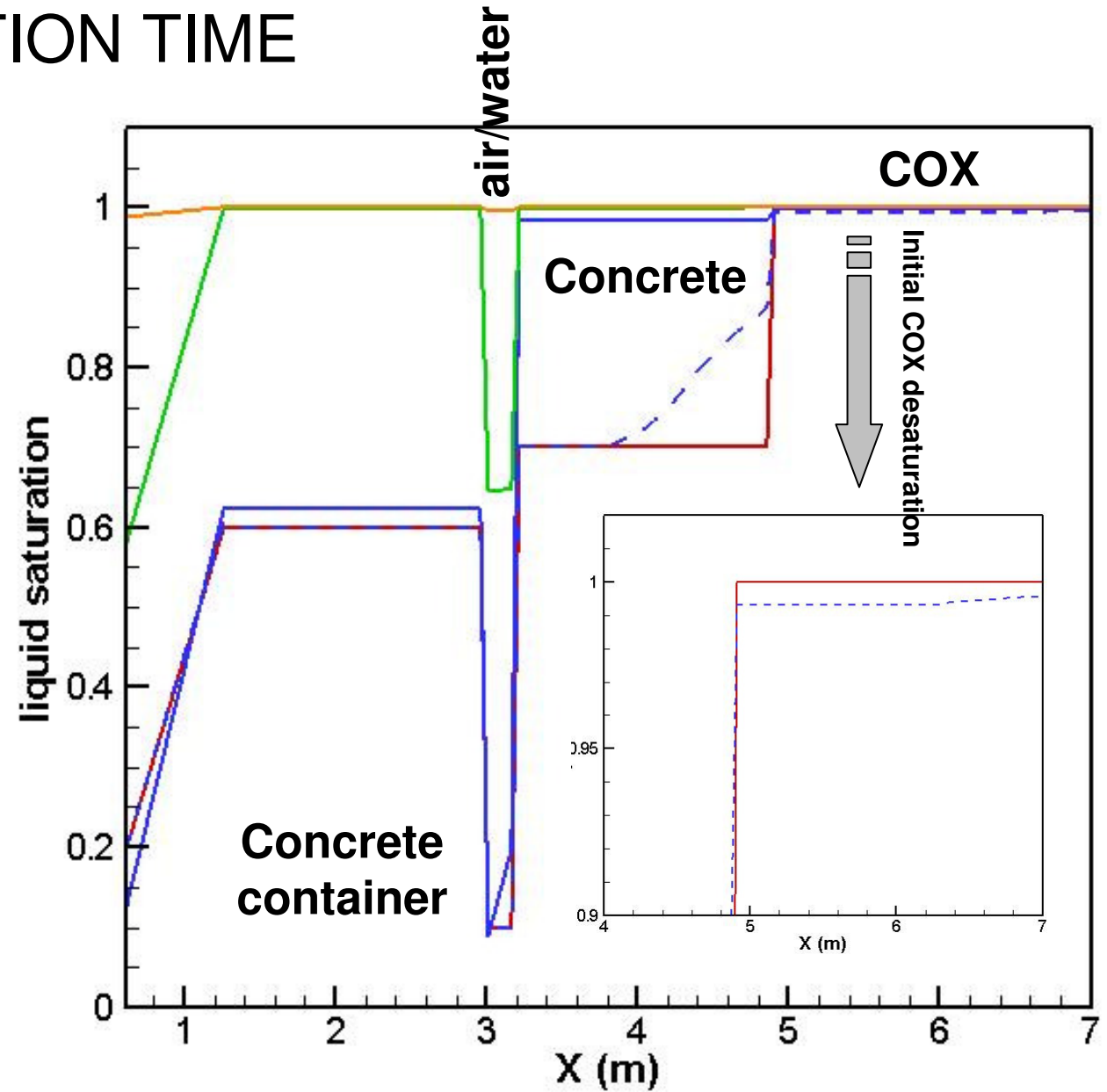
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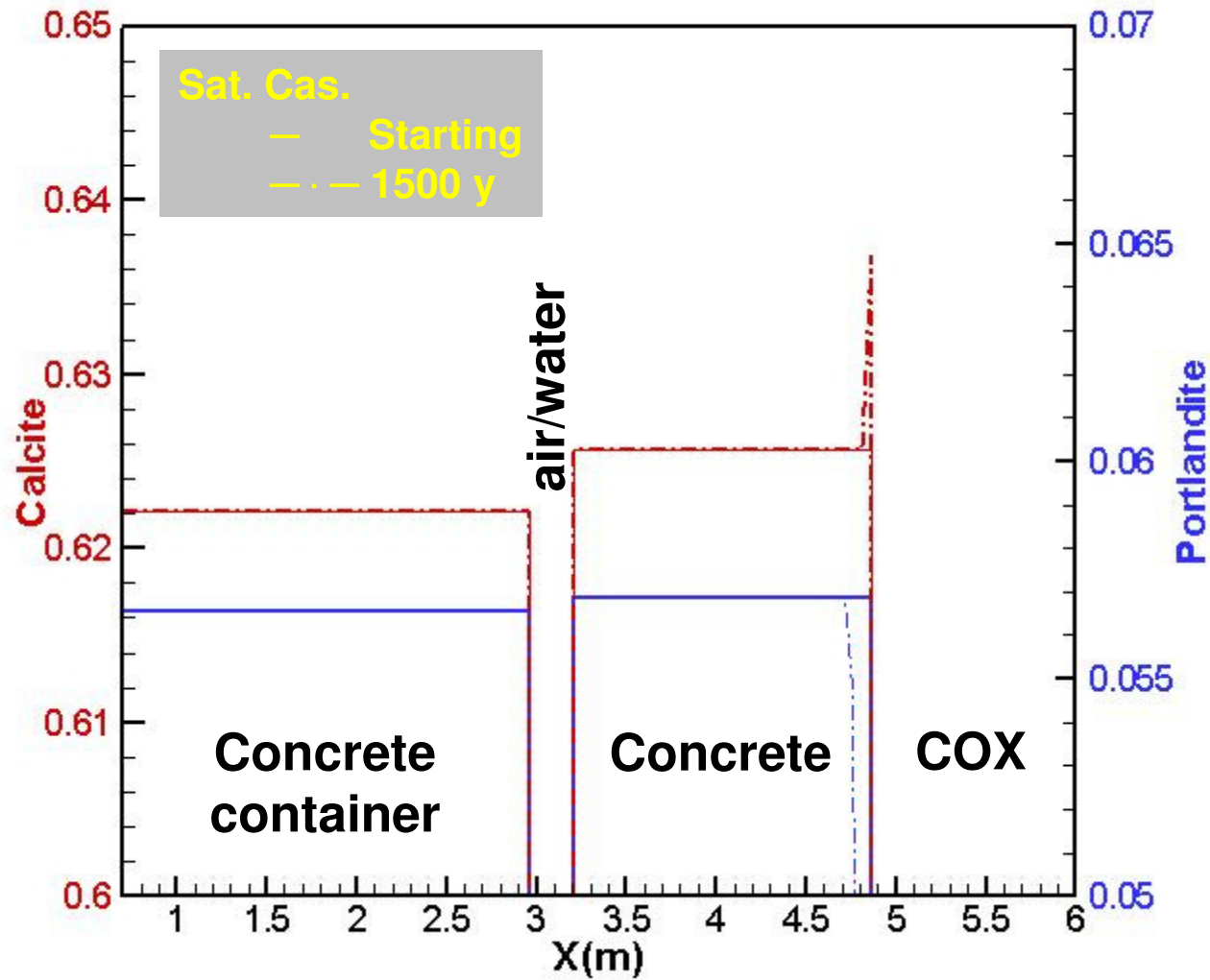
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RESATURATION TIME

- Initial
- 0.1 y
- 100 y
- 500 y
- 1000 y

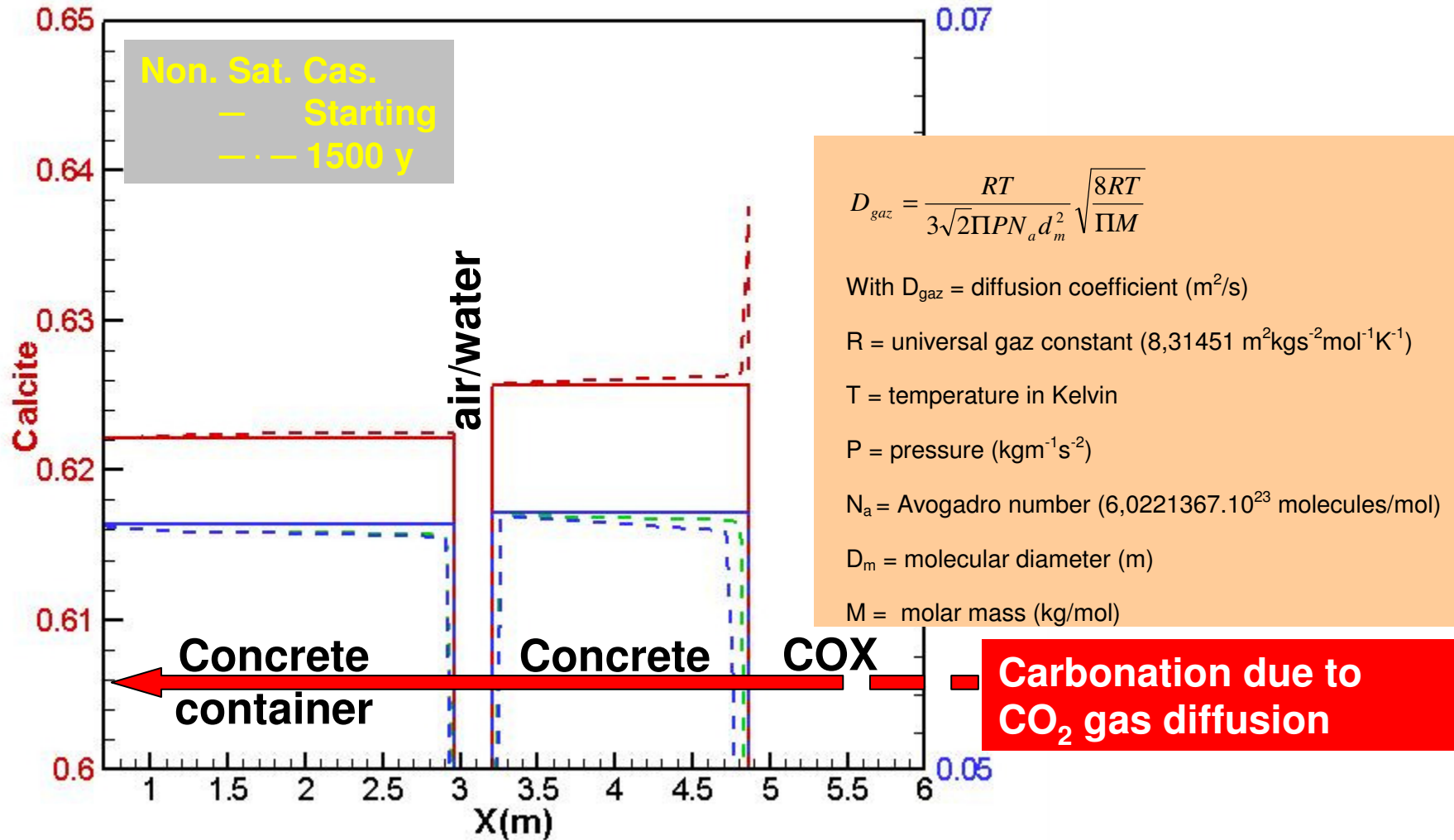


SATURATED CONDITIONS



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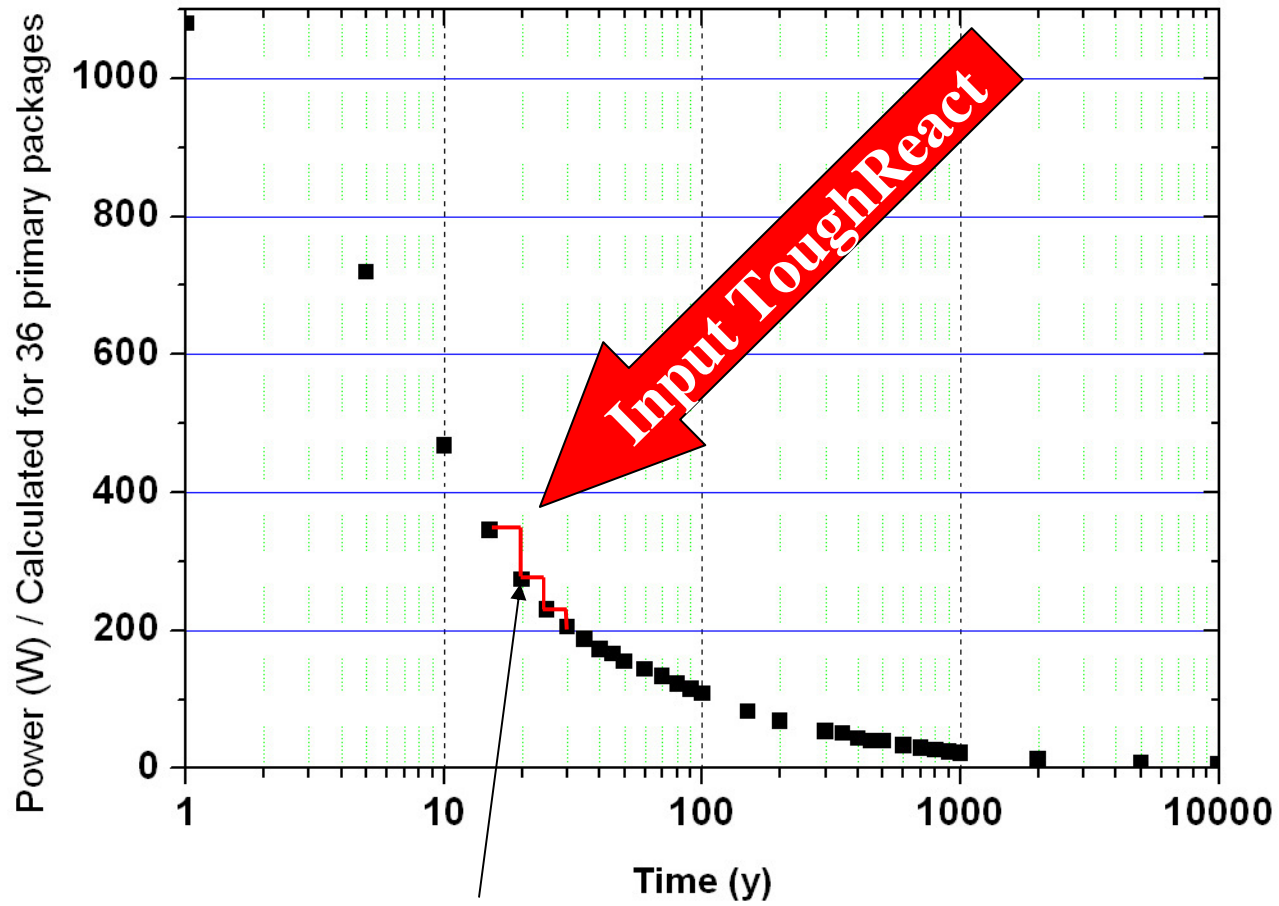
NON SATURATED CONDITIONS



CRITICAL ELEMENTS FOR THE MODELLING

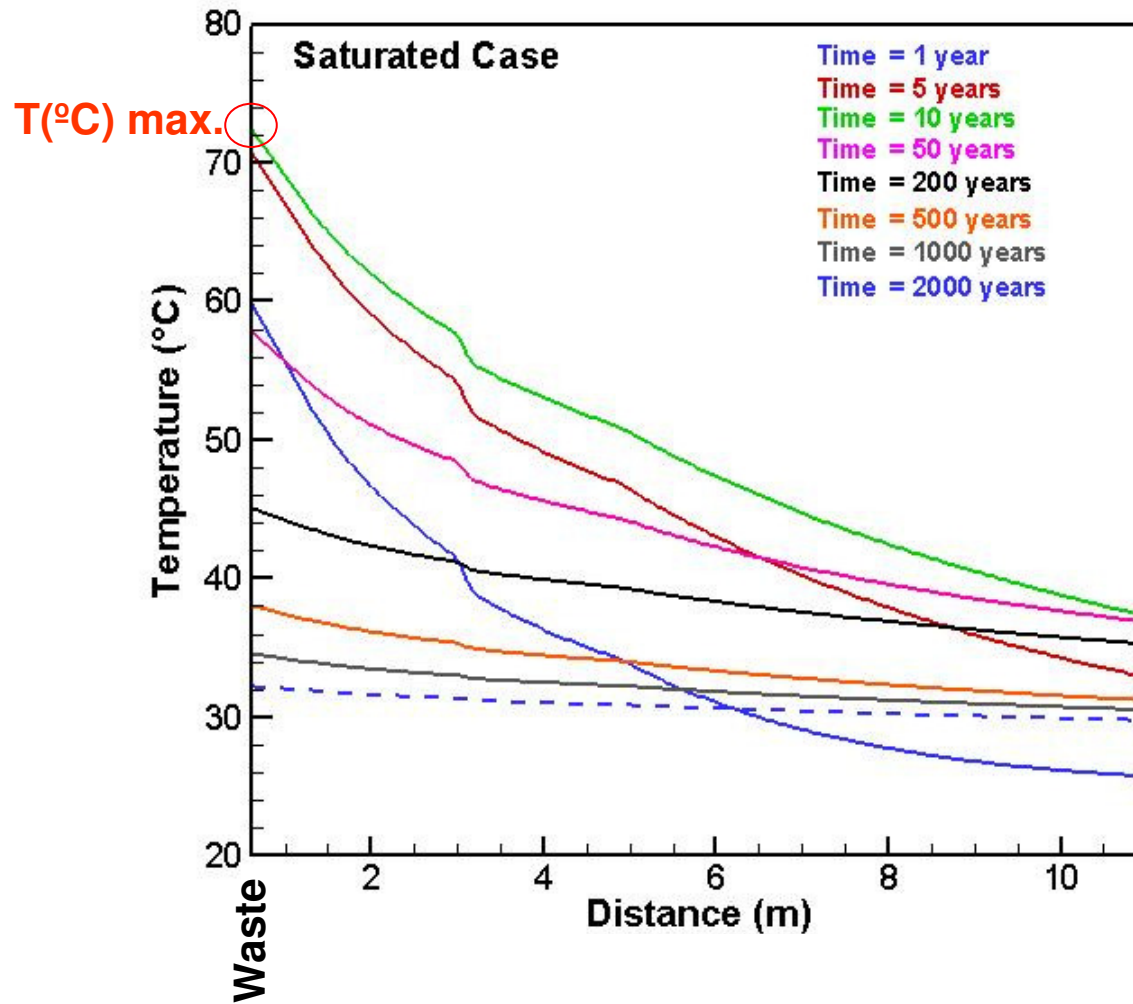
- > A coherent thermodynamic database to work in temperature
- > A “complete” mineralogical description of the initial system
- > Transport parameters (porosities, permeabilities, diffusion coefficients, heat conductivities...)
- > **Transport reactive calculation**
 - PHREEQC (1D)
 - TOUGHREACT (radial geometry, non saturated condition, thermal gradient....)
- > Experiments to test and improve the modelling
- >

TRANSIENT THERMAL STATE



270 W after 20 years

TEMPERATURE EVOLUTION



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CONCLUSIONS

- > Alteration of concrete/clay: limited in space (~50cm) with saturated conditions and clogging**
- > Clogging porosity is mesh size dependent at local equilibrium**
- > Transient states (non-saturated period, thermal period) : ~ 2000 years**
- > Carbonation: increased by CO₂(g) diffusion in non-saturated conditions**

OUTLOOK

- > Fully coupled reactive transport considering complex mineralogy and complex geometry with both non-saturated and non-isothermal conditions**
- > Simulation of fractures of EDZ (due to excavation) by “Multiple Interacting Continua” (MINC function of TOUGH2)**
- > Kinetics instead of local equilibrium**
- > Archie law: retroaction of chemical reactions on effective diffusion coefficient**

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